

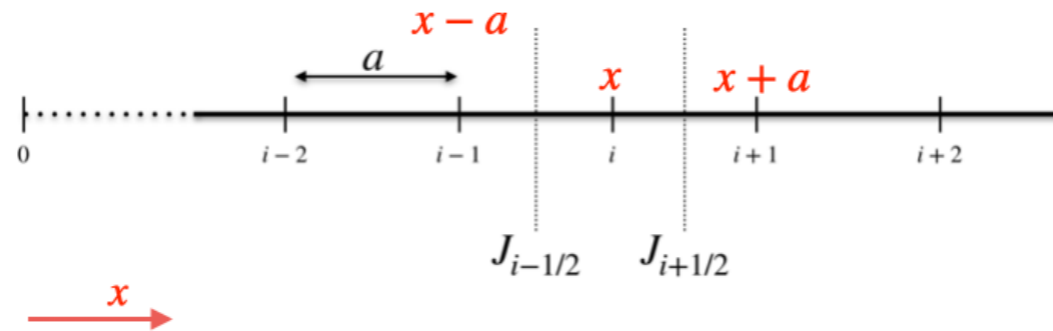
# **ChE-402: Diffusion and Mass Transfer**

## Lecture 2

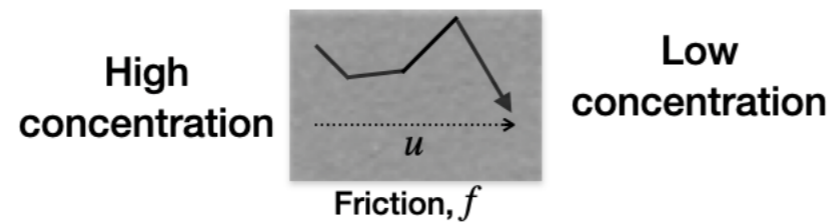
# Intended Learning Outcomes

To apply mass balance using Fick's law to predict time-independent (steady-state) and time-dependent (unsteady state or transient) evolution of concentration profile.

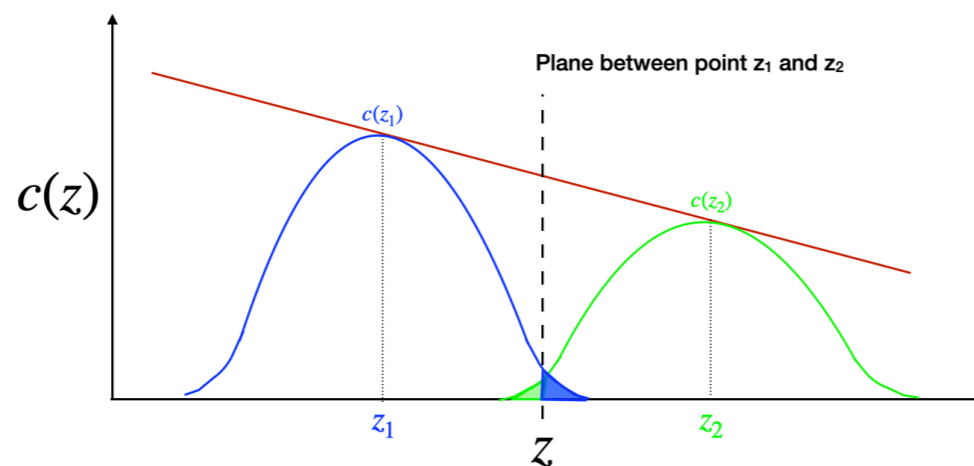
# Three interpretation on origin of diffusion



$$D = \frac{\Gamma a^2}{2}$$



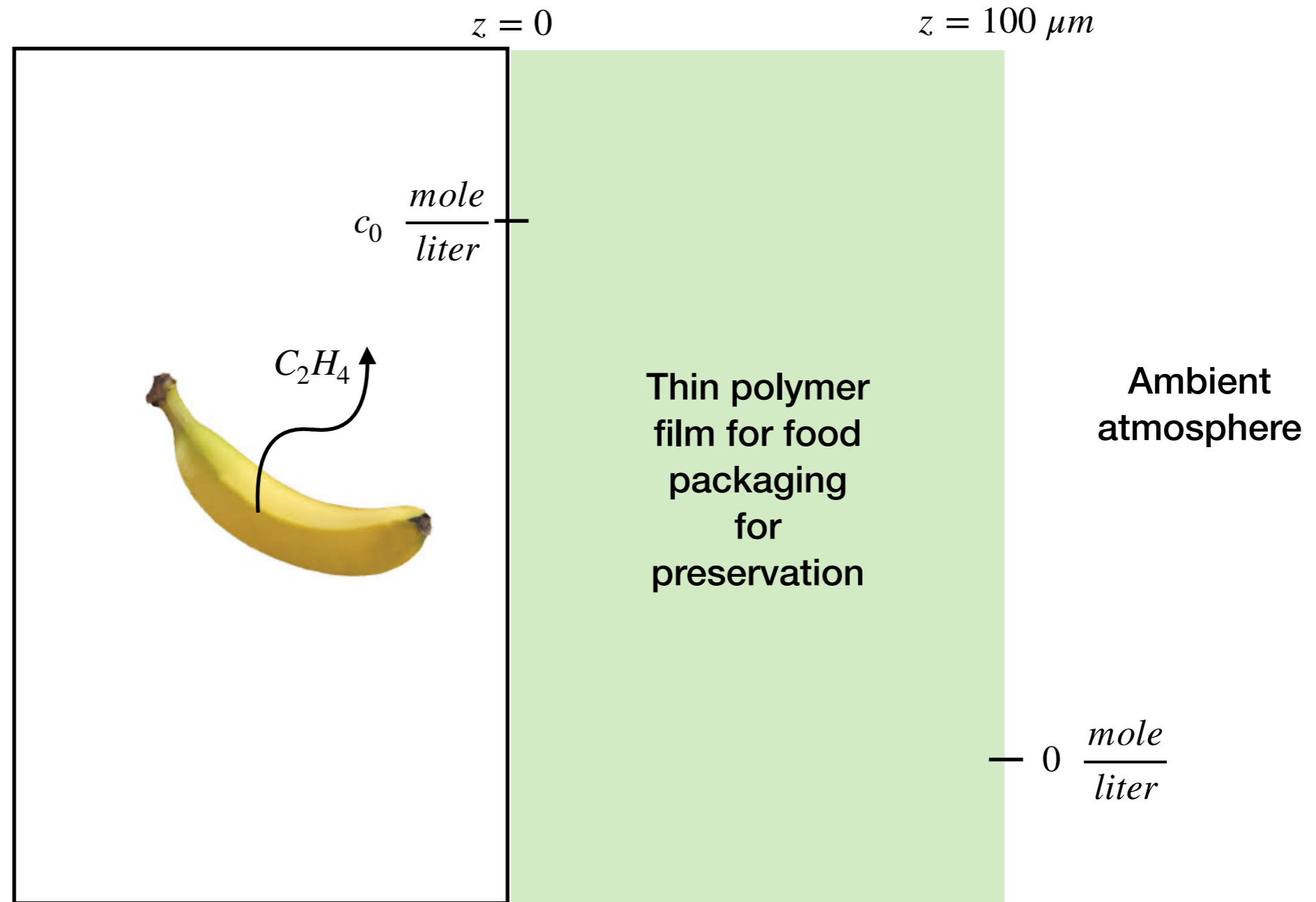
$$D_o = \frac{k_B T}{f}$$



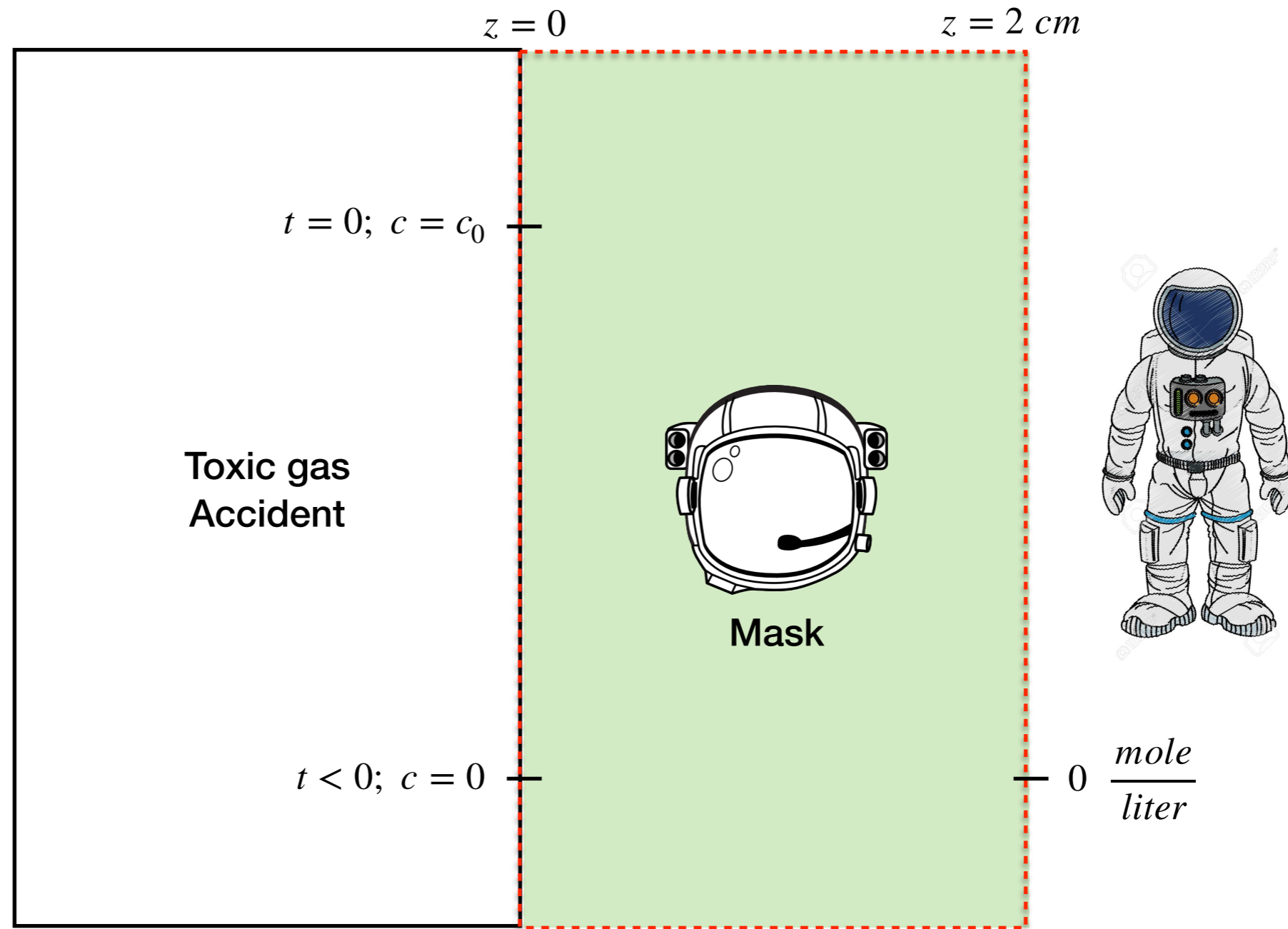
$$N(z, t) = \frac{N_o(t = 0, z_0)}{\sqrt{4\pi D_o t}} \exp\left(\frac{-z^2}{4D_o t}\right)$$

$$J = -D \frac{\partial c(x, t)}{\partial x}$$

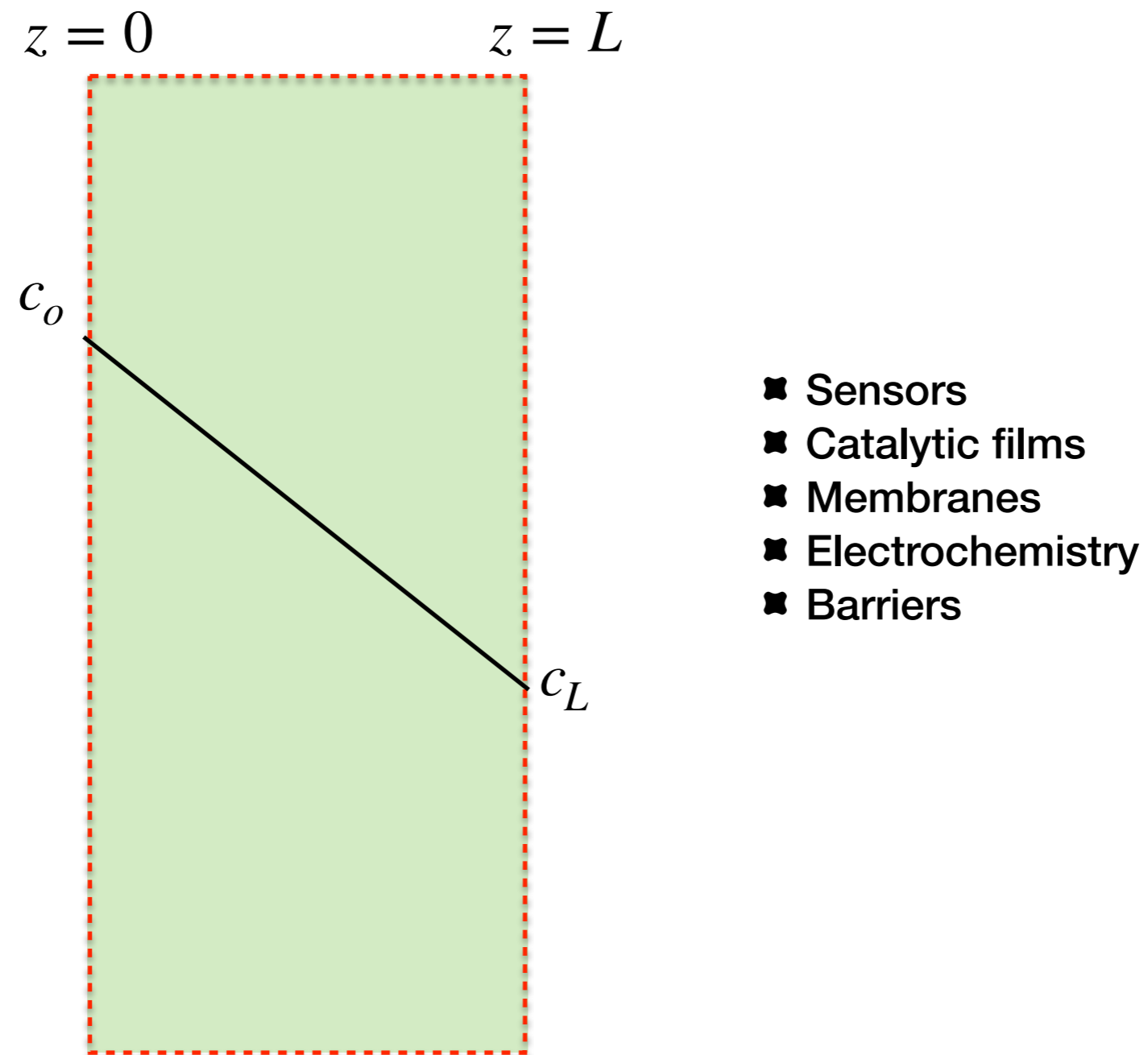
How can we describe the flux of  $C_2H_4$  from the food packaging film to make sure food is not wasted?



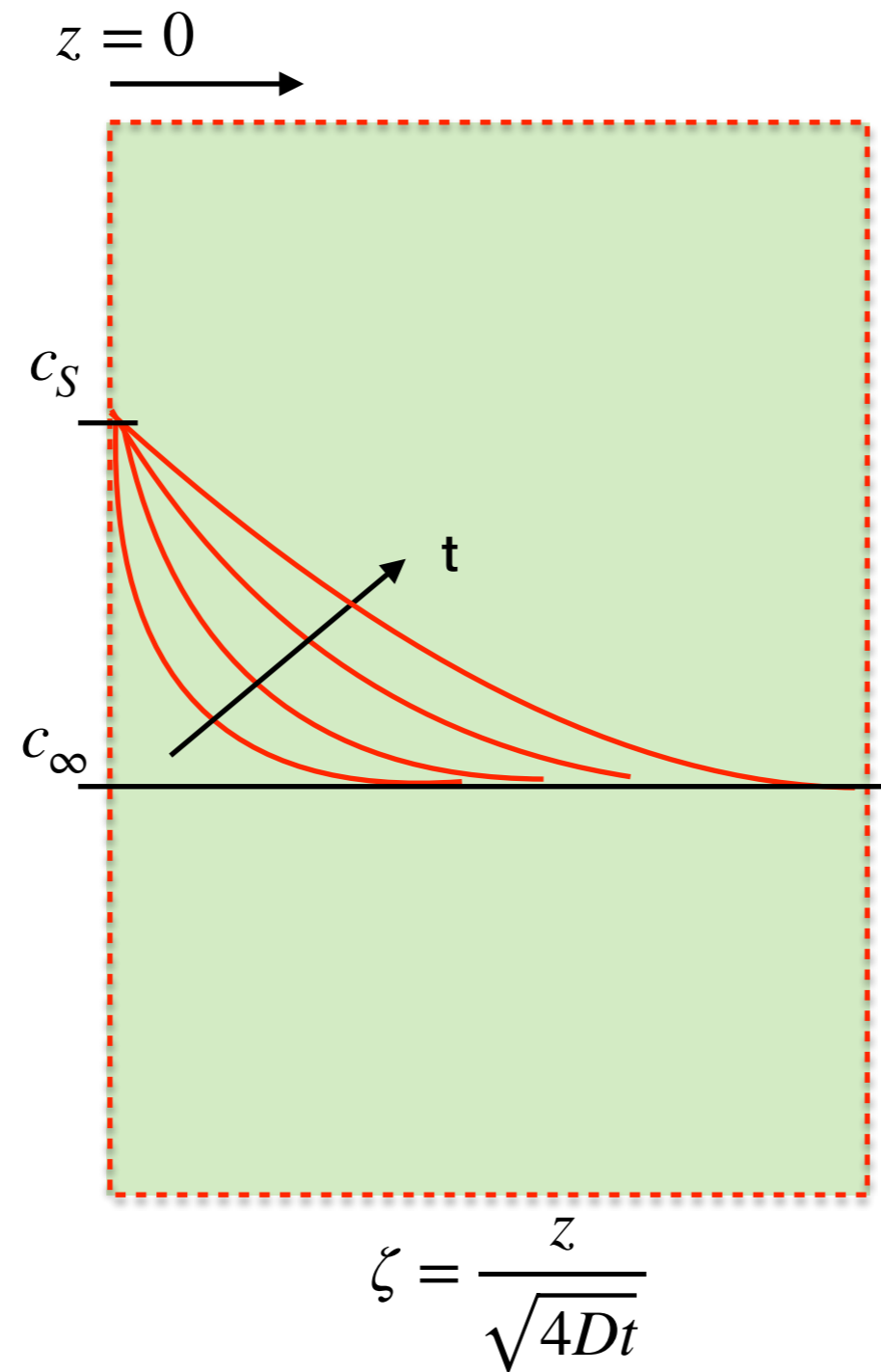
How can we calculate the time that an astronaut has to fix the accident before toxic gas reaches critical concentration,  $c_{toxic}$  inside the mask ?



# Steady-state diffusion across a thin film



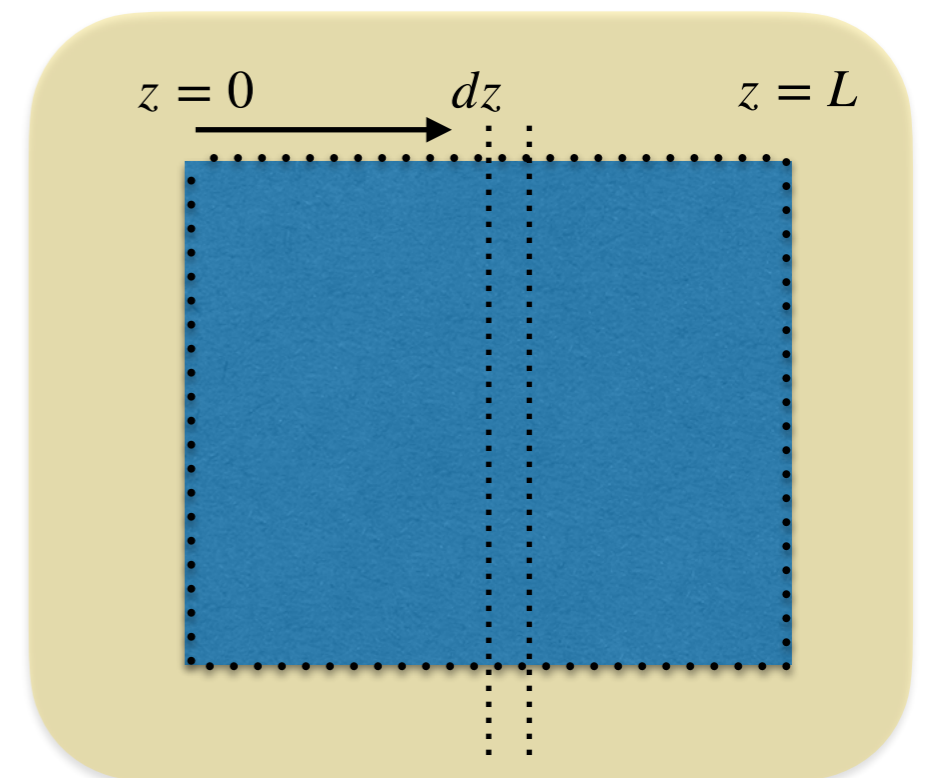
# Transient diffusion across a semi-infinite slab



# Approach to solve diffusion problems

1. Define your system.
2. Identify boundary and initial conditions.
3. Choose an element with volume,  $dV$ , where you will do mass balance
4. Apply mass balance on the element.
5. Apply transport, reaction and thermodynamic laws in the mass balance.
6. Apply boundary and initial condition.

Diffusion across the blue box



# Steady-state diffusion across a thin film - generic case

**Define your system:** the thin film

**2 boundary conditions:**  $c = c_0$  at  $z = 0$        $c = c_L$  at  $z = L$

**Choose an element with volume,  $dV$ , to do mass balance**

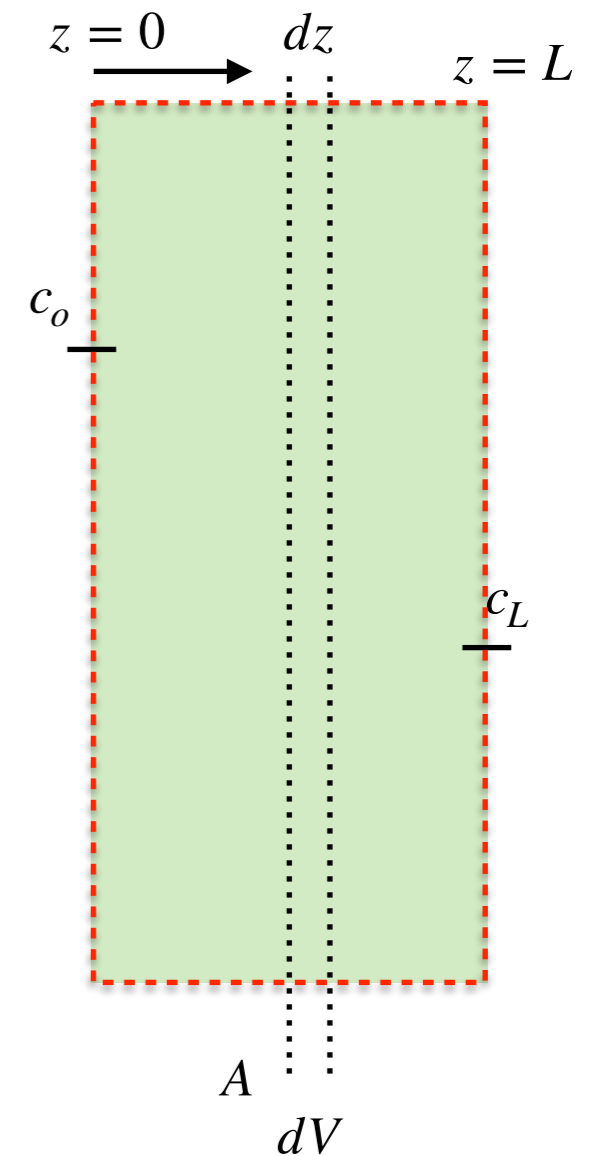
$$\overset{\circ}{Accumulation} * dV = \overset{\circ}{Flux} |_{in} * A - \overset{\circ}{Flux} |_{out} * A + \overset{\circ}{Generation} * dV - \overset{\circ}{Consumption} * dV$$

$$dV = Adz$$

$$Adz \frac{dc}{dt} = AJ |_z - AJ |_{z+dz} + 0 \text{ (no reaction)} - 0 \text{ (no reaction)}$$

$$\frac{dc}{dt} = \frac{J |_z - J |_{z+dz}}{dz}$$

$$\text{Steady-state; } \Rightarrow \frac{dc}{dt} = 0$$



Concentration is uniform along the width of the film

Cross-sectional area = A

# Steady-state diffusion across a thin film - generic case

$$0 = \frac{J|_z - J|_{z+dz}}{dz}$$

$$0 = - \left( \frac{J|_{z+dz} - J|_z}{(z+dz) - z} \right)$$

$$0 = - \frac{d}{dz} J$$

Apply transport law; we can use Fick's law here with constant D

$$J = -D \frac{dc}{dz}$$

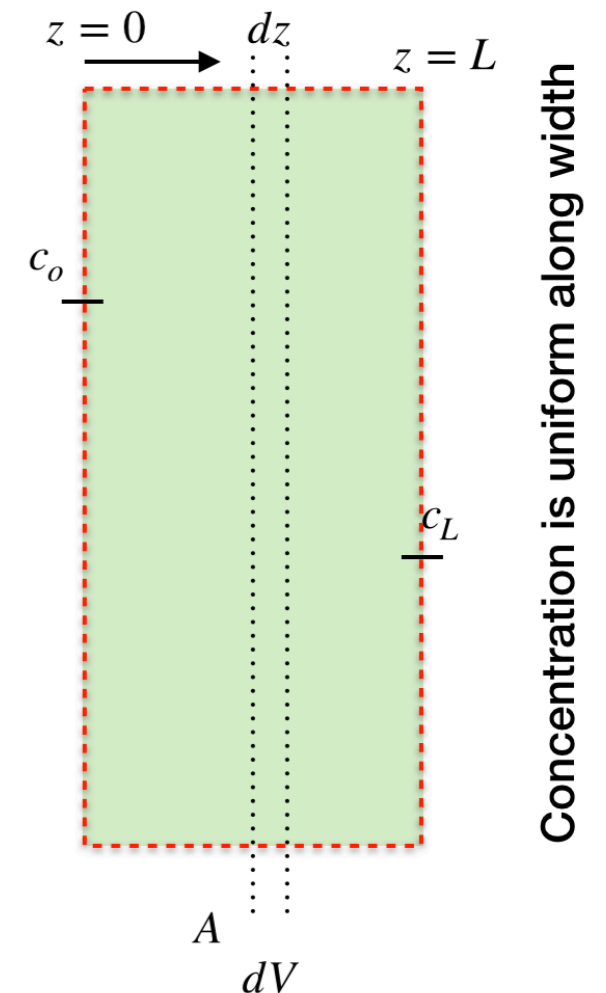
$$0 = D \frac{d^2c}{dz^2}$$

Solve using the 2 boundary conditions  $c = c_0$  at  $z = 0$        $c = c_L$  at  $z = L$

$$\frac{dc}{dz} = \text{constant} = S_1$$

$$c = S_1 z + S_2 \text{ where } S_2 \text{ is another constant}$$

$$c = c_0 + (c_L - c_0) \frac{z}{L}$$



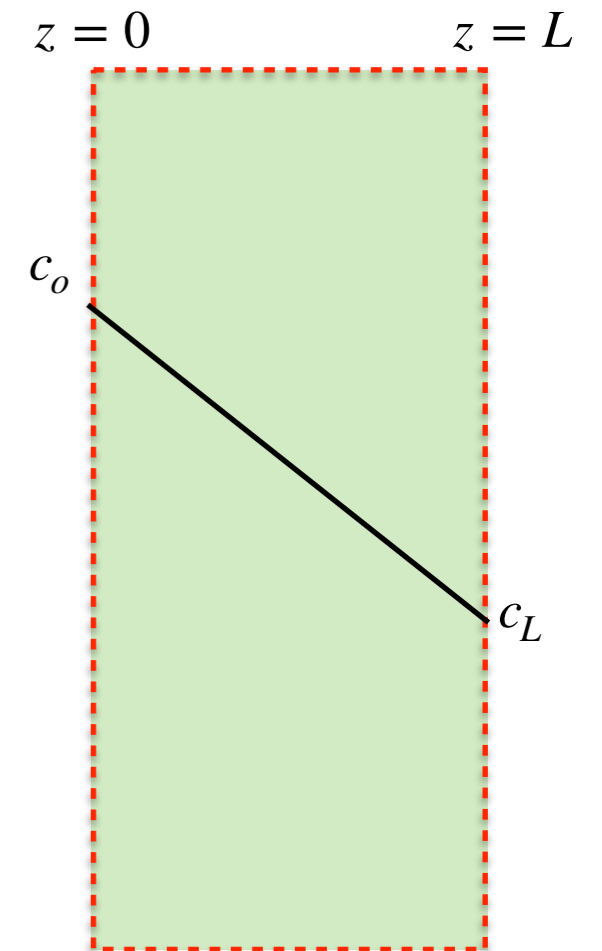
# Steady-state diffusion across a thin film - generic case

$$c = c_0 + (c_L - c_0)\frac{z}{L}$$

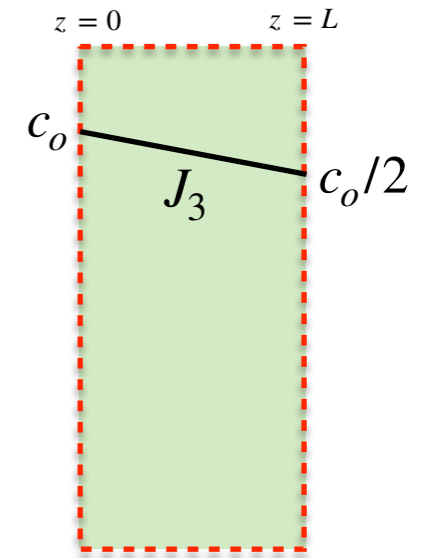
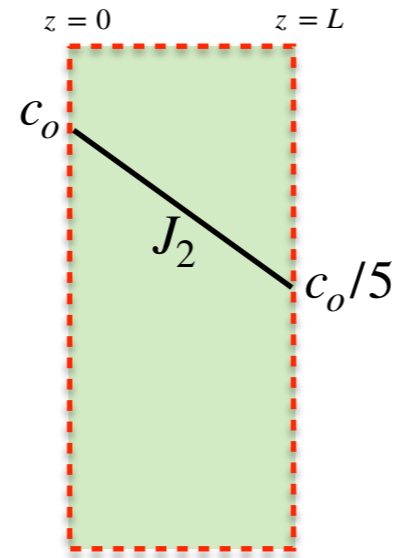
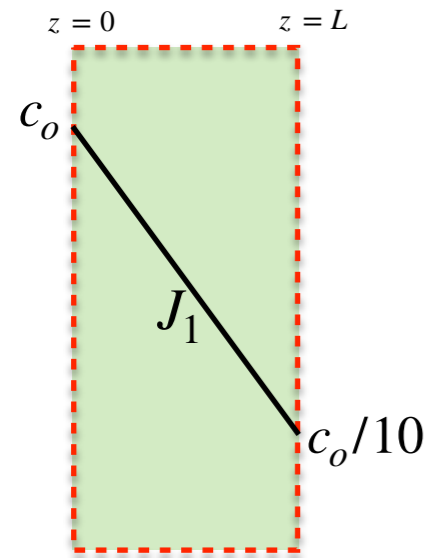
Can you calculate flux,  $J$  ?

$$J = -D\frac{dc}{dz} = D\frac{(c_0 - c_L)}{L} = \text{constant}$$

$$0 = -\frac{d}{dz}J$$



Rank the flux when the diffusivity is same in all cases.



A)  $J_1 = J_2 = J_3$

B)  $J_1 > J_2 > J_3$

C)  $J_1 < J_2 < J_3$

D) Not sufficient evidence

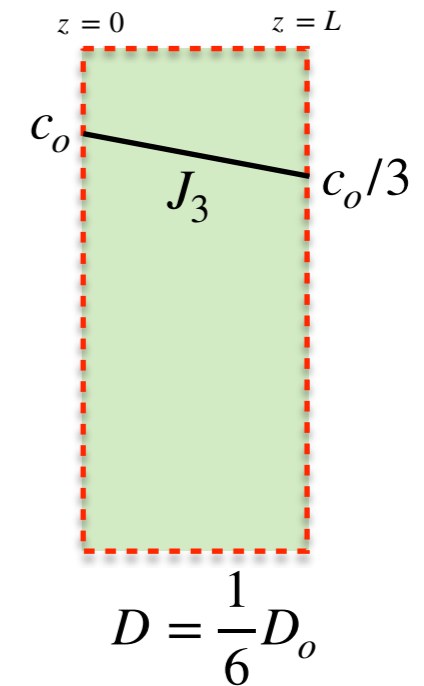
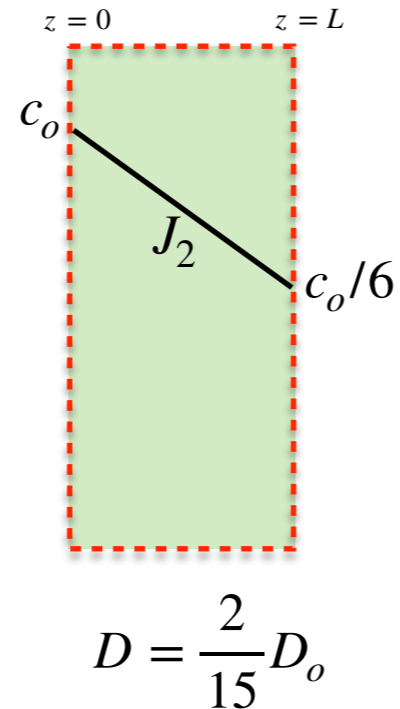
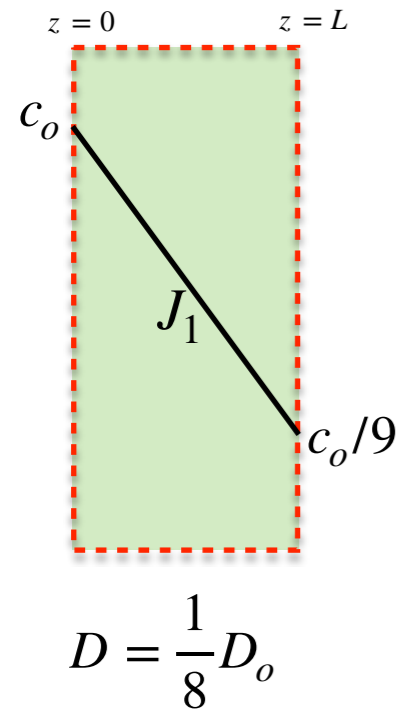
$J$  is proportional to  $\Delta C$  because  $D$  and  $L$  are fixed

$$J_1 \propto 9/10c_0$$

$$J_2 \propto 8/10c_0$$

$$J_3 \propto 5/10c_0$$

Rank the flux when the diffusivity is not same in all cases.



$J$  is proportional to  $\Delta C$  and  $D$ ;  $L$  is fixed

A)  $J_1 = J_2 = J_3$

B)  $J_1 > J_2 > J_3$

C)  $J_1 < J_2 < J_3$

D) Not sufficient evidence

$$J_1 \propto 1/9 D_0 c_0$$

$$J_2 \propto 1/9 D_0 c_0$$

$$J_3 \propto 1/9 D_0 c_0$$

# Steady-state diffusion across a thin film - generic case

For the following case, calculate

- 1) Concentration at  $z = 30$  and  $70 \mu\text{m}$
- 2) Flux at  $z = 30$  and  $z = 70 \mu\text{m}$

Concentration profile is linear

At  $z = 30 \mu\text{m}$

$$c = c_0 + (c_L - c_0) \frac{z}{L}$$

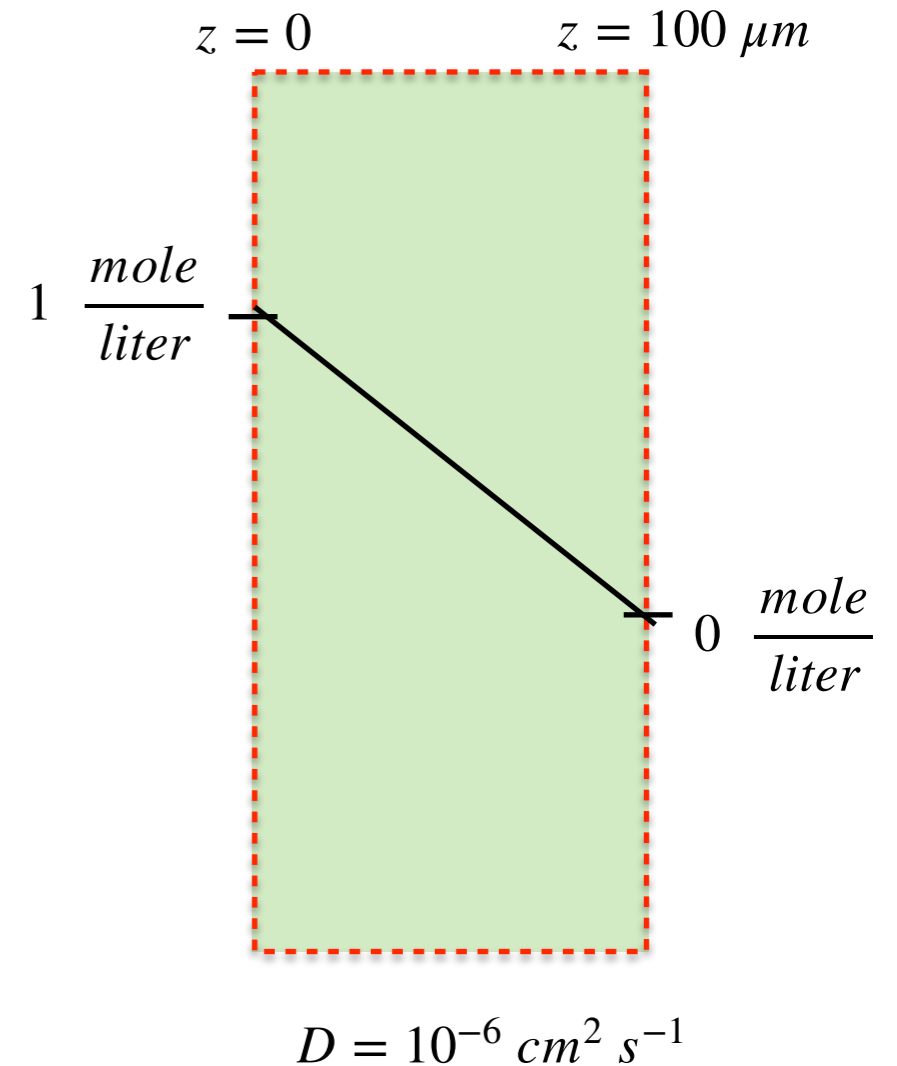
$$\Rightarrow c = 1 + (0 - 1) \frac{30}{100} \frac{\text{mole}}{\text{liter}} = 0.7 \frac{\text{mole}}{\text{liter}}$$

At  $z = 70 \mu\text{m}$

$$c = c_0 + (c_L - c_0) \frac{z}{L}$$

$$\Rightarrow c = 1 + (0 - 1) \frac{70}{100} \frac{\text{mole}}{\text{liter}} = 0.3 \frac{\text{mole}}{\text{liter}}$$

$$J = -D \frac{dc}{dz} = D \frac{(c_0 - c_L)}{L} = \text{constant}$$



$$J = 10^{-10} \frac{(1000 - 0)}{10^{-4}} = 10^{-3} \frac{\text{mole}}{\text{m}^2 \text{ s}}$$

# Steady-state diffusion across a thin membrane

**Additional considerations here:**

What is the difference with the previous case ?

**How would you solve this problem?**

**Apply thermodynamics to calculate boundary conditions**

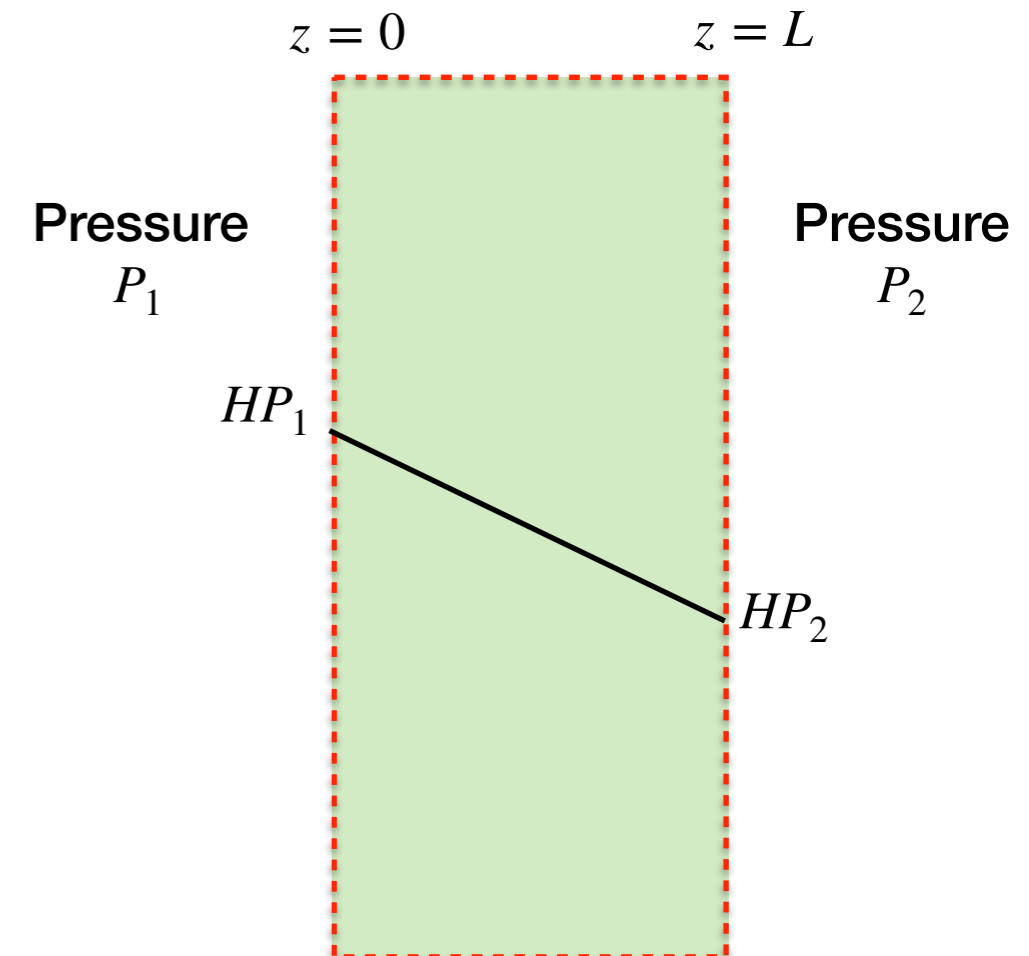
For dilute case, one can use Henry's law of adsorption

$$c|_{z=0} = HP_1 \qquad c|_{z=L} = HP_2$$

**Can you derive the rest??**

$$c = c_0 + (c_L - c_0)\frac{z}{L} = HP_1 + H(P_2 - P_1)\frac{z}{L}$$

$$J = -D\frac{dc}{dz} = D\frac{(c_0 - c_L)}{L} = D\frac{(HP_1 - HP_2)}{L} = \text{constant}$$



# Calculate $c_i$ at the steady-state

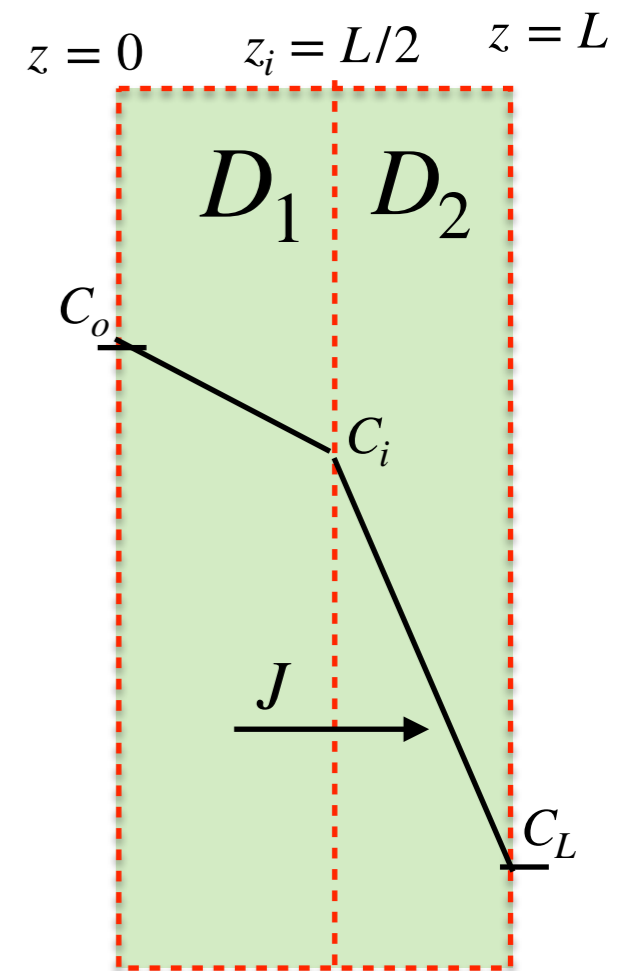
$$J = J_{\text{left}} = J_{\text{right}}$$

$$-D_1 \frac{(c_0 - c_i)}{z_i} = -D_2 \frac{(c_i - c_L)}{z_L - z_i}$$

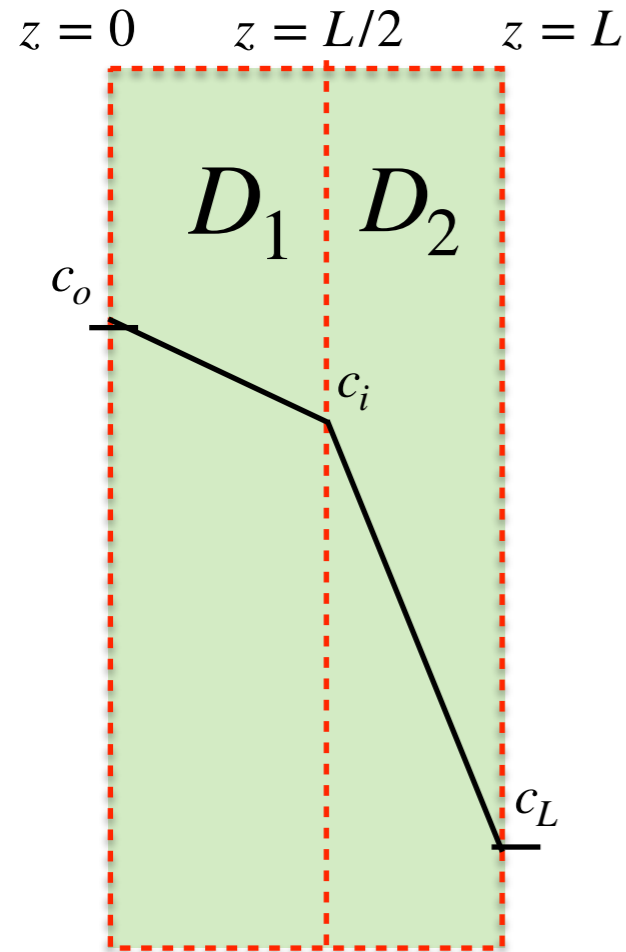
$$\Rightarrow c_0 - c_i = (c_i - c_L) \left( \frac{D_2}{D_1} \frac{z_i}{z_L - z_i} \right)$$

$$= (c_i - c_L) \left( \frac{D_2}{D_1} \right)$$

$$\Rightarrow c_i = \frac{c_0 + c_L \left( \frac{D_2}{D_1} \right)}{1 + \left( \frac{D_2}{D_1} \right)}$$



What is the relation between  $D_1$  and  $D_2$  at the steady state?



A)  $D_1 = D_2$

B)  $D_1 > D_2$

C)  $D_1 < D_2$

D) Not sufficient evidence

$J_1 = J_2$  at the steady state.

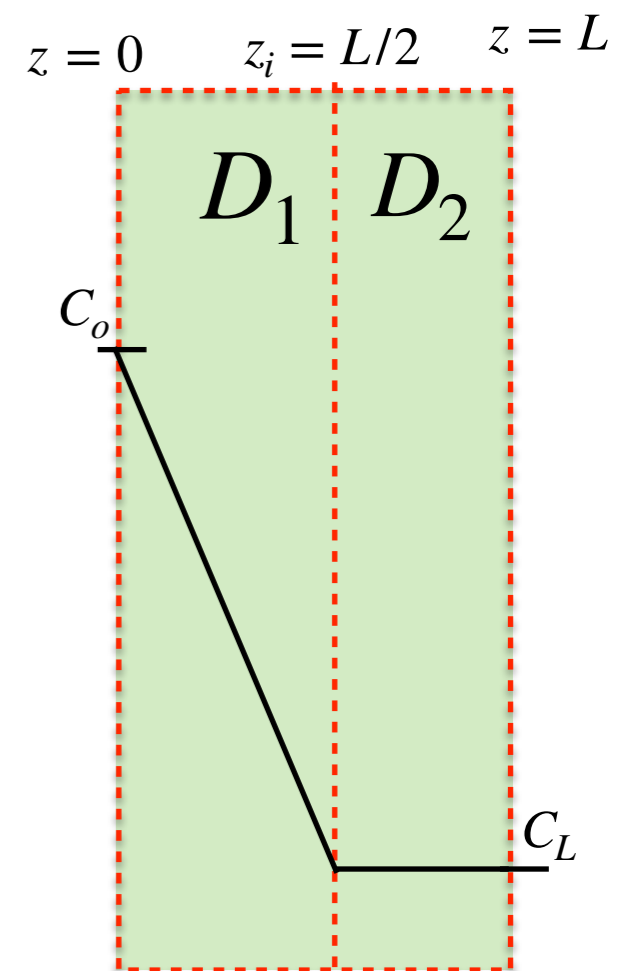
$$\Rightarrow D_1(c_0 - c_i) = D_2(c_i - c_L)$$

$$\Rightarrow \frac{D_1}{D_2} = \frac{(c_i - c_L)}{(c_0 - c_i)}$$

$$\Rightarrow \frac{D_1}{D_2} > 1$$

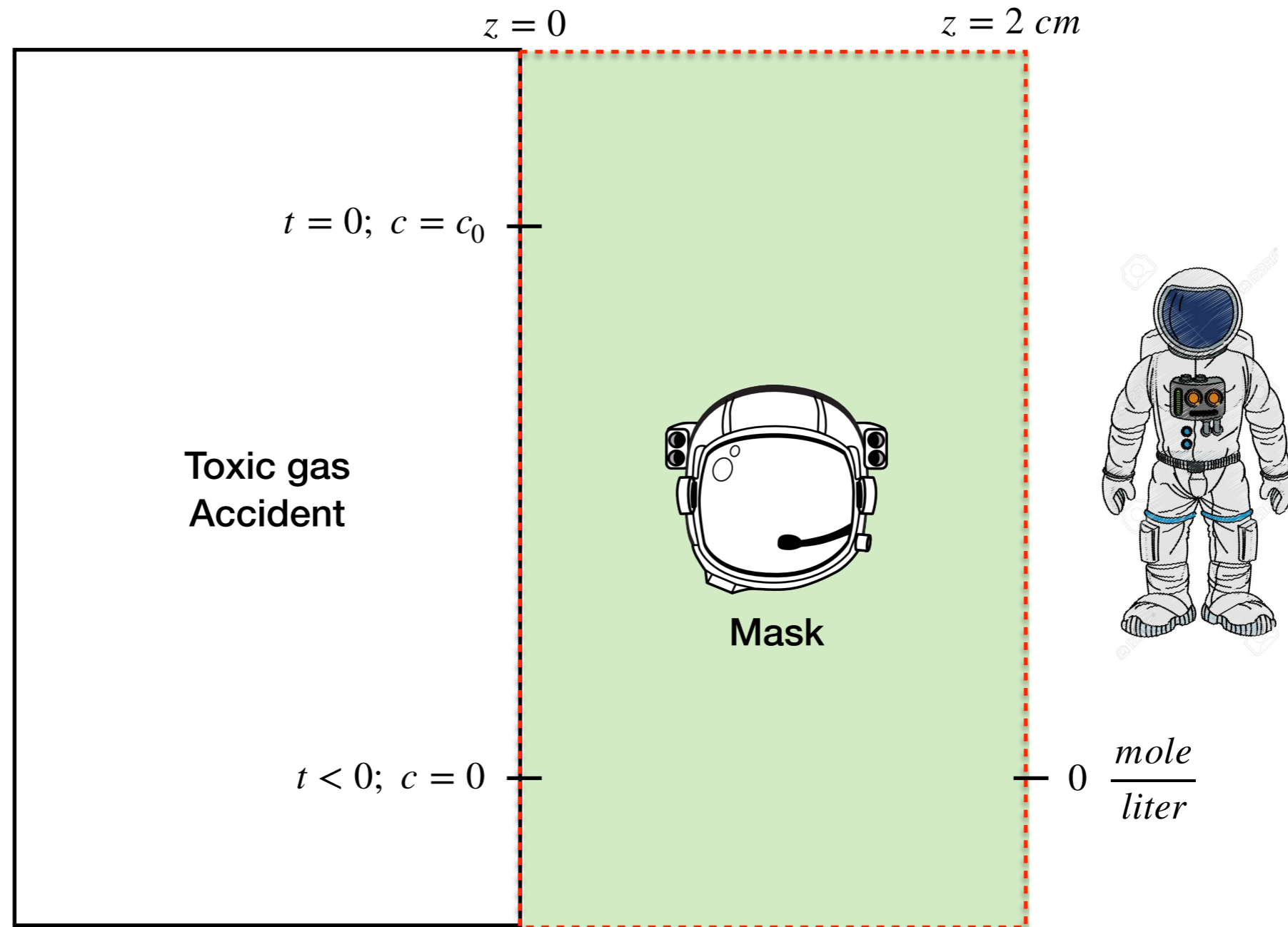
Draw concentration profiles at steady-state:

$$D_1 = 0.05 \text{ cm}^2/\text{s}, \quad D_2 = \infty$$



How can we calculate the time that an astronaut has to fix the issue before toxic gas reaches toxic concentration,

$c_{toxic}$



# Transient diffusion across a semi-infinite slab

**Initial condition:**  $t = 0, c = c_\infty$

The concentration at left face ( $z=0$ ) is suddenly raised to  $C_s$  at  $t=0$

**Define your system:** The slab

**Define an elemental volume to do mass balance:**  $dV = Adz$

**Apply mass balance**

$$\overset{o}{Accumulation} * dV = \overset{o}{Flux} |_{in} * A - \overset{o}{Flux} |_{out} * A + \overset{o}{Generation} * dV - \overset{o}{Consumption} * dV$$

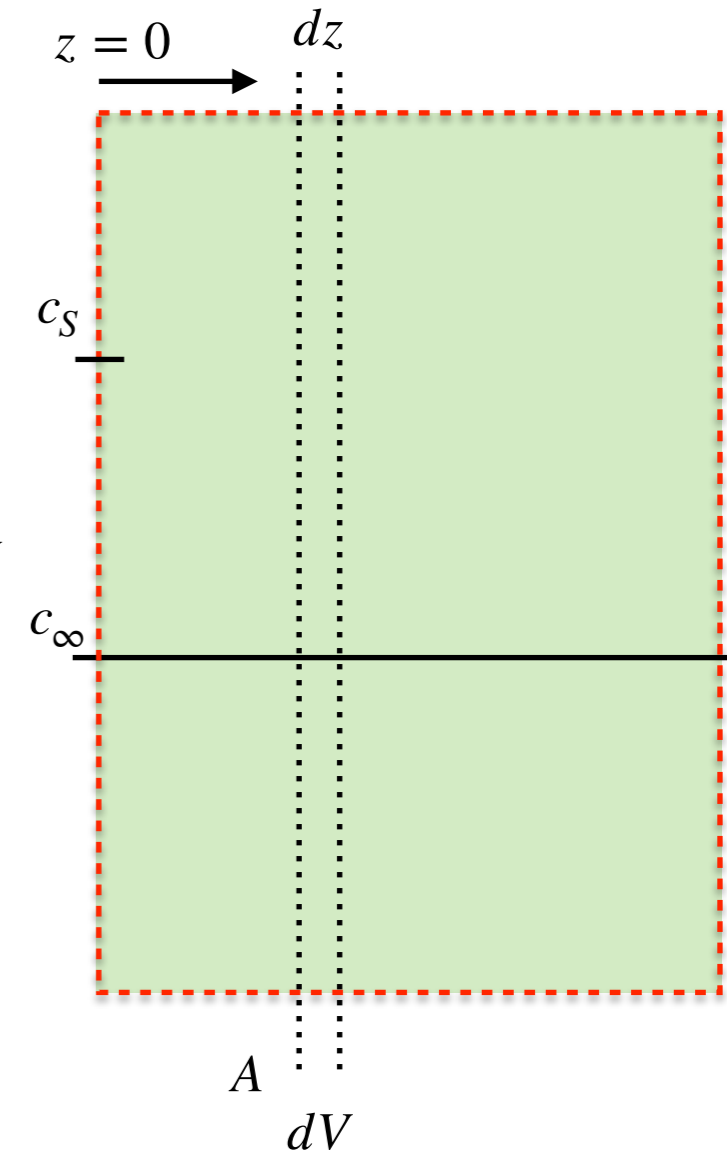
$$Adz \frac{\partial c}{\partial t} = AJ |_z - AJ |_{z+dz} + 0 \text{ (no reaction)} - 0 \text{ (no reaction)}$$

$$\Rightarrow \frac{\partial c}{\partial t} = \frac{J |_z - J |_{z+dz}}{dz} = - \frac{\partial J}{\partial z}$$

$$\Rightarrow \frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial z^2}$$

**Boundary conditions:**

$$t > 0 \quad c |_{z=0} = c_s; \quad c |_{z=\infty} = c_\infty$$



# Transient diffusion across a semi-infinite slab

$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial z^2}$$

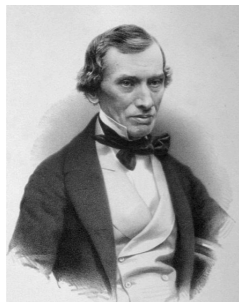
**Initial condition:**  $t = 0, c = c_\infty$

**Boundary conditions:**  $t > 0 \quad c|_{z=0} = c_S; c|_{z=\infty} = c_\infty$

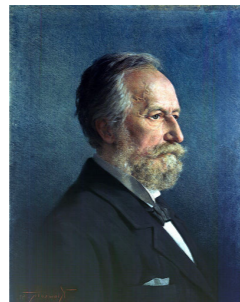
**Search of solution:**



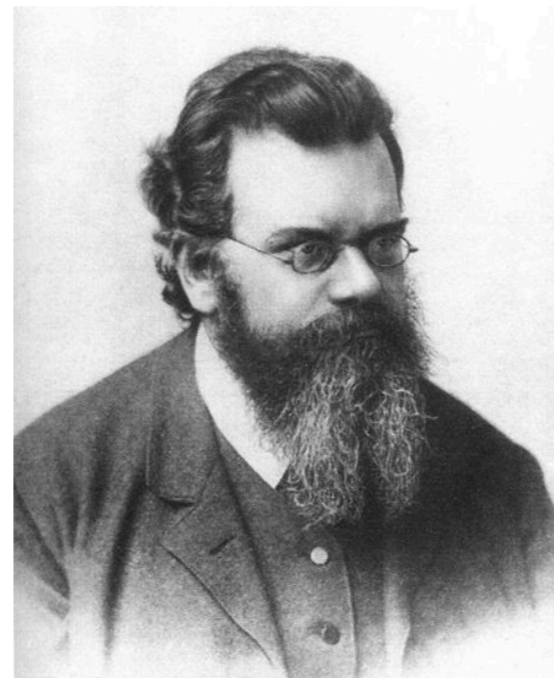
Fourier



Graham



Fick



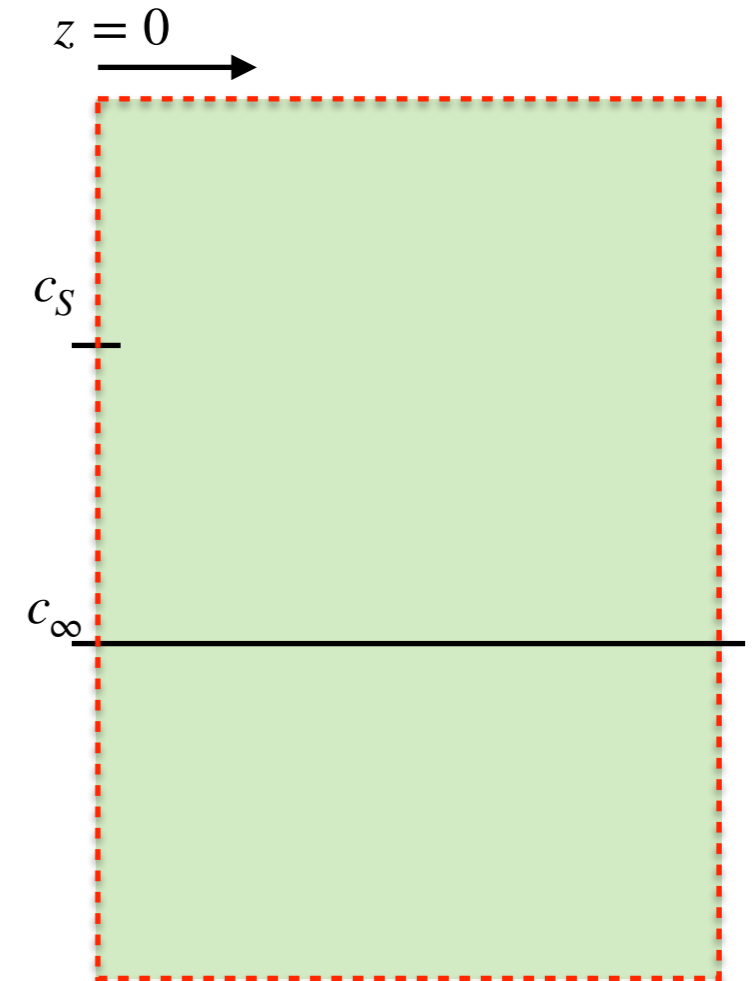
**Ludwig Boltzmann**  
using combination of variable

$$\zeta = \frac{z}{\sqrt{4Dt}} \quad c = c(\zeta)$$

$$\Rightarrow \frac{dc}{d\zeta} \left( \frac{\partial \zeta}{\partial t} \right) = D \frac{d^2 c}{d\zeta^2} \left( \frac{\partial \zeta}{\partial z} \right)^2$$

$$\Rightarrow \frac{dc}{d\zeta} \left( \frac{z}{-2t\sqrt{4Dt}} \right) = D \frac{d^2 c}{d\zeta^2} \left( \frac{1}{\sqrt{4Dt}} \right)^2$$

$$\Rightarrow \frac{d^2 c}{d\zeta^2} + 2\zeta \frac{dc}{d\zeta} = 0$$



# Transient diffusion across a semi-infinite slab

$$\frac{d^2c}{d\zeta^2} + 2\zeta \frac{dc}{d\zeta} = 0 \quad \zeta = \frac{z}{\sqrt{4Dt}}$$

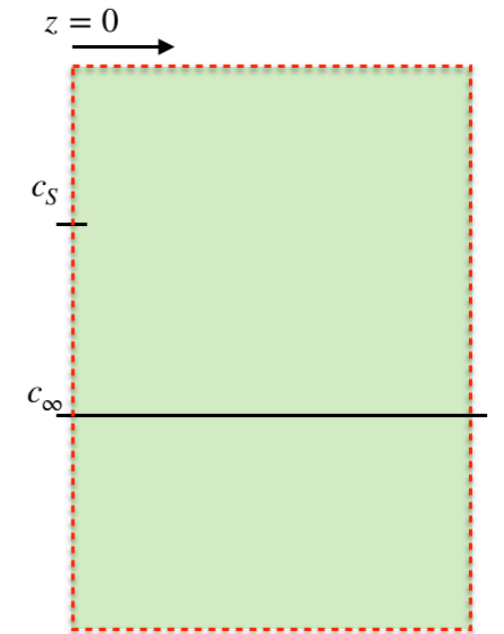
**Boundary conditions:**  $t > 0$

$$c|_{z=0} = c_S$$

$$c|_{\zeta=0} = c_S;$$

$$c|_{z=\infty} = c_\infty$$

$$c|_{\zeta=\infty} = c_\infty$$



**First Integration**

$$\text{assume } \frac{dc}{d\zeta} = Q \quad \Rightarrow \frac{dQ}{d\zeta} + 2\zeta Q = 0 \quad \Rightarrow \int \frac{dQ}{Q} = -2 \int \zeta d\zeta \quad \Rightarrow \ln Q = -\zeta^2 + \text{constant}$$

$$\Rightarrow Q = W \exp(-\zeta^2)$$

**2nd Integration**

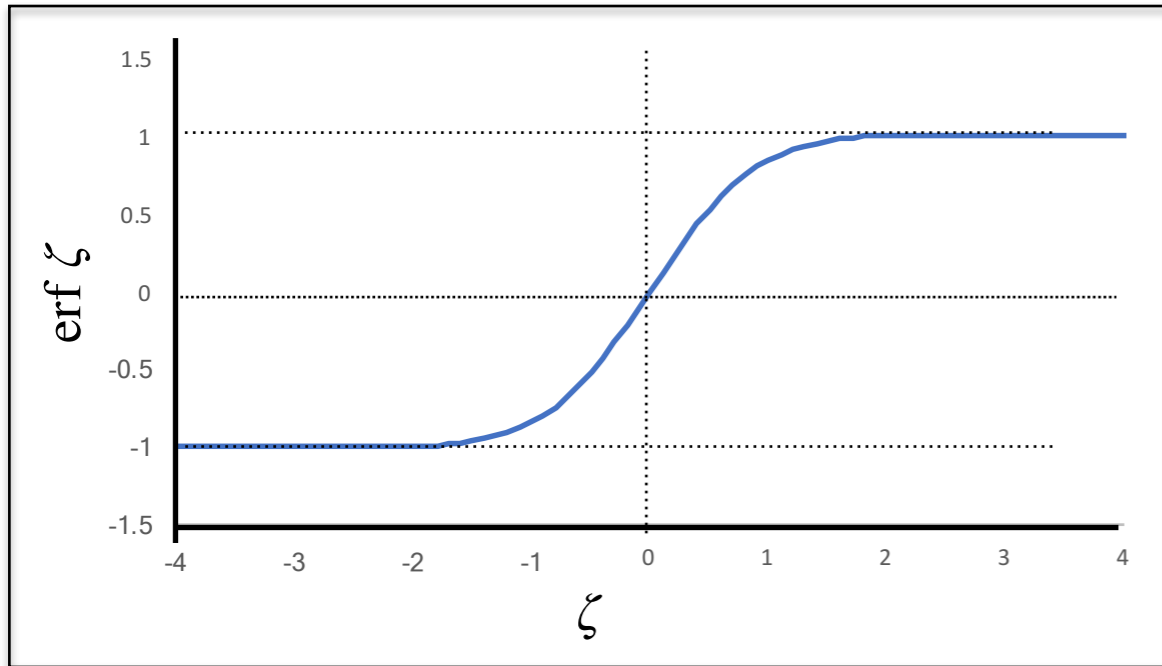
$$\int dc = \int Q d\zeta \quad \Rightarrow \int dc = \int W \exp(-\zeta^2) d\zeta \quad \Rightarrow c = \frac{\sqrt{\pi}}{2} W \operatorname{erf} \zeta + \bar{W}$$

$$\text{where, } \operatorname{erf} \zeta = \frac{2}{\sqrt{\pi}} \int_0^\zeta \exp(-r^2) dr$$

# Transient diffusion across a semi-infinite slab

$$c = \frac{\sqrt{\pi}}{2} W \operatorname{erf} \zeta + \bar{W}$$

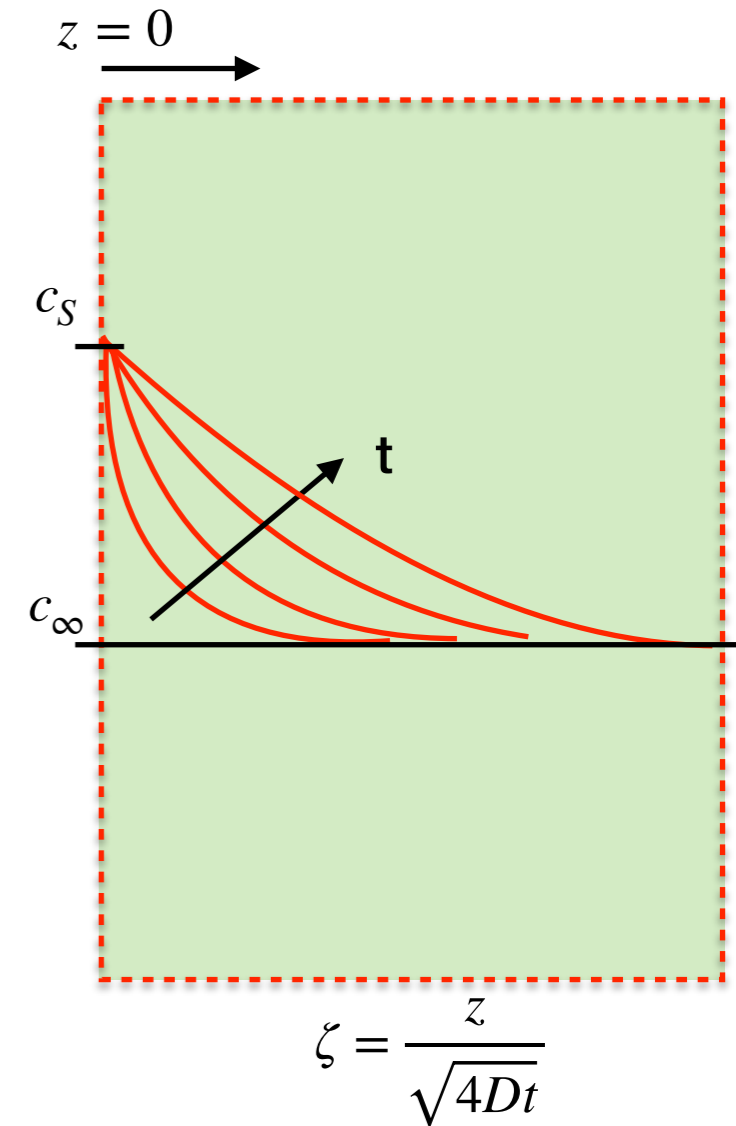
$$\operatorname{erf} \zeta = \frac{2}{\sqrt{\pi}} \int_0^\zeta \exp(-r^2) dr$$



**Boundary conditions:**

$$c|_{\zeta=0} = c_S;$$

$$c|_{\zeta=\infty} = c_\infty$$



**Applying boundary conditions**

$$\bar{W} = c_S$$

$$W = \frac{2}{\sqrt{\pi}} (c_\infty - c_S)$$

$$\frac{c(z, t) - c_S}{c_\infty - c_S} = \operatorname{erf} \zeta = \frac{2}{\sqrt{\pi}} \int_0^\zeta \exp(-r^2) dr$$

$$\frac{c_1 - c_{10}}{c_{1\infty} - c_{10}} = \operatorname{erf} \zeta$$

# Calculation of flux for transient diffusion

$$\frac{c(z, t) - c_S}{c_\infty - c_S} = \operatorname{erf} \zeta = \frac{2}{\sqrt{\pi}} \int_0^\zeta \exp(-r^2) dr$$

$$J = -D \frac{\partial c}{\partial z}$$

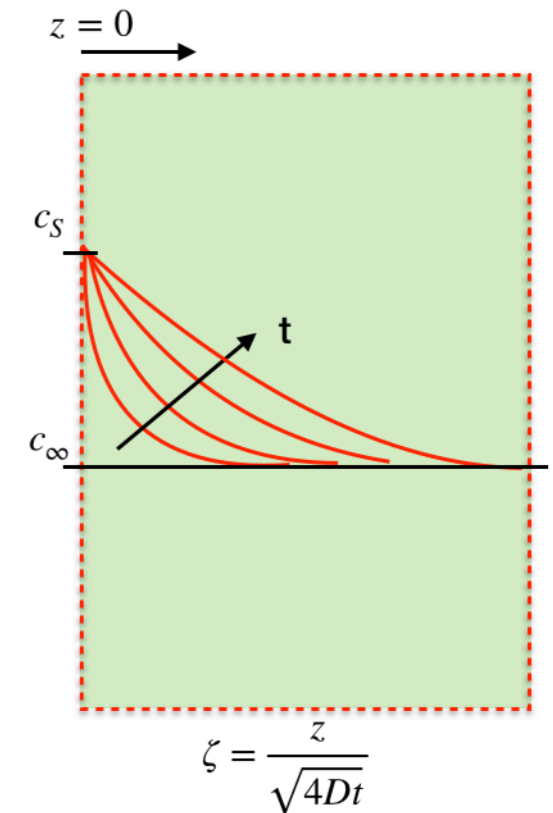
$$\frac{\partial c}{\partial z} = \left( \frac{dc}{d\zeta} \right) \left( \frac{\partial \zeta}{\partial z} \right)$$

$$\frac{dc}{d\zeta} = (c_\infty - c_S) d(\operatorname{erf} \zeta) = (c_\infty - c_S) \frac{2}{\sqrt{\pi}} \exp\left(-\frac{z^2}{4Dt}\right)$$

$$\zeta = \frac{z}{\sqrt{4Dt}} \quad \Rightarrow \quad \left( \frac{\partial \zeta}{\partial z} \right) = \frac{1}{\sqrt{4Dt}}$$

$$\Rightarrow \frac{\partial c}{\partial z} = (c_\infty - c_S) \frac{1}{\sqrt{\pi Dt}} \exp\left(-\frac{z^2}{4Dt}\right)$$

$$\Rightarrow J = -D \frac{\partial c}{\partial z} = -\sqrt{\frac{D}{\pi t}} (c_\infty - c_S) \exp\left(-\frac{z^2}{4Dt}\right)$$

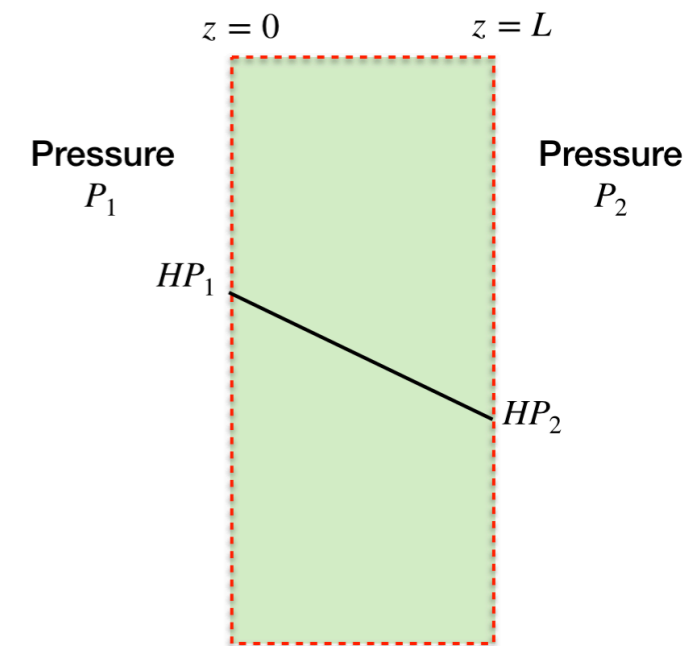


# Exercise 1: steady-state diffusion across a thin membrane

A plastic bag is designed to increase the shelf life of bananas. It works by removing ethylene responsible for ripening bananas. The bag is made of 1  $\mu\text{m}$  thick polymer film. Assuming that the concentration of ethylene outside the bag (in the room) is zero, and inside the bag is 1 mole%, calculate grams of ethylene that would be removed in 1 day from a bag made of 1  $\text{m}^2$  material. The pressure inside and outside the bag is 1 bar.

$$H = 0.1 \frac{\text{mol}}{\text{liter bar}}$$

$$D = 10^{-6} \text{ cm}^2 \text{ s}^{-1}$$



# Exercise 1 solution

A plastic bag is designed to increase the shelf life of bananas. It works by removing ethylene responsible for ripening bananas. The bag is made of 1  $\mu\text{m}$  thick polymer film. Assuming that the concentration of ethylene outside the bag (in the room) is zero, and inside the bag is 1 mole%, calculate grams of ethylene that would be removed in 1 day from a bag made of 1  $\text{m}^2$  material. The pressure inside and outside the bag is 1 bar.

$$H = 0.1 \frac{\text{mol}}{\text{liter bar}}$$

$$D = 10^{-6} \text{ cm}^2 \text{ s}^{-1}$$

Inner wall of bag, ethylene concentration =  $HP_1 = 0.1 * 0.01 = 0.001 \frac{\text{mol}}{\text{liter}}$

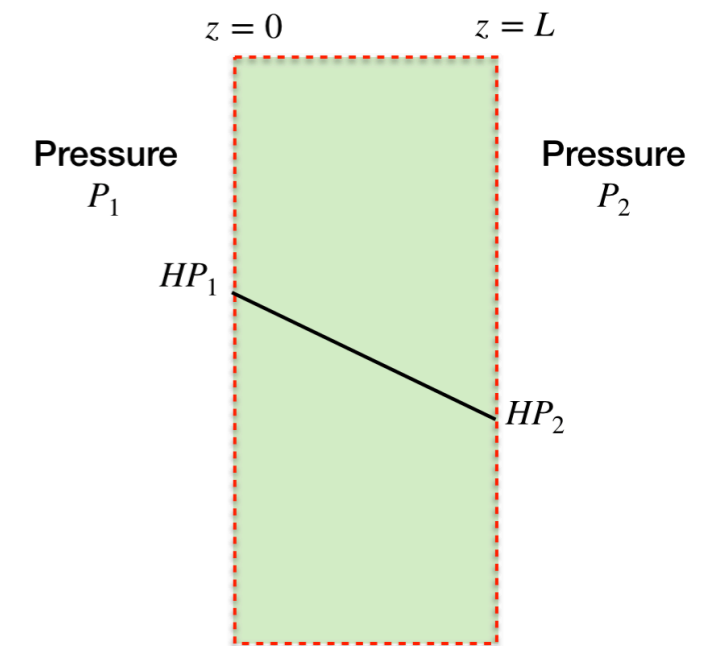
Outer wall of bag, ethylene concentration =  $HP_2 = 0 \frac{\text{mol}}{\text{liter}}$

$$J = -D \frac{dc}{dz} = D \frac{(HP_1 - HP_2)}{L} = \text{constant}$$

$$J = 10^{-10} \frac{(1 - 0)}{10^{-6}} = 10^{-4} \frac{\text{mole}}{\text{m}^2 \text{s}}$$

$$\text{moles removed} = 10^{-4} * 1 * 24 * 3600 = 8.64 \text{ mole}$$

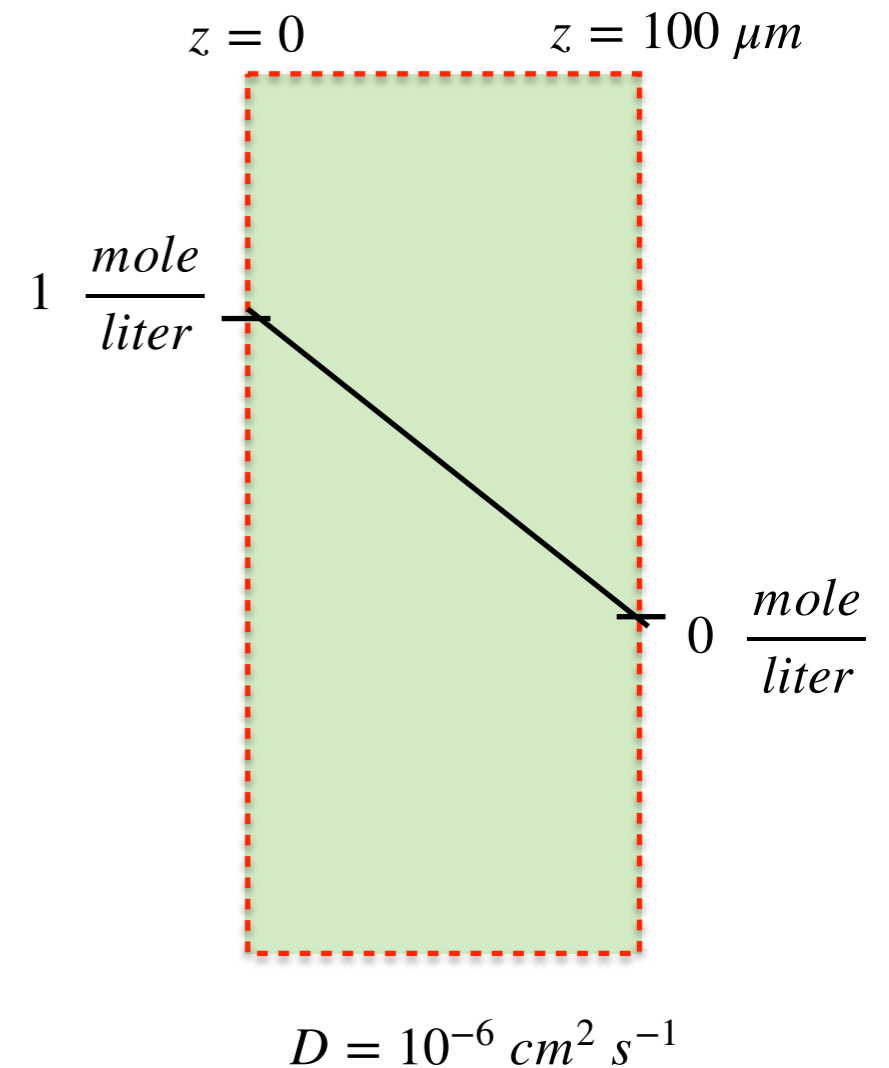
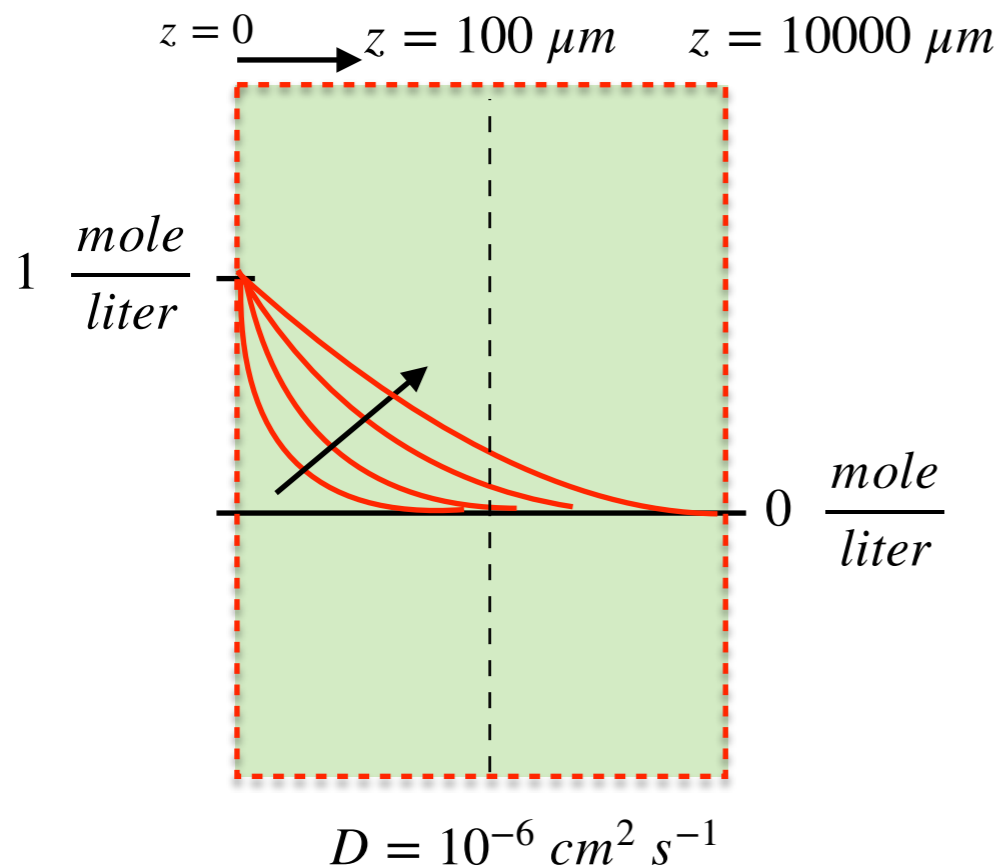
$$\text{gram removed} = 8.64 * 28 \text{ g} = 241.9 \text{ gm}$$



# Exercise 2: Compare the flux in transient vs. steady-state case

Calculate flux at  $z = 100 \mu\text{m}$  at  $t = 1 \text{ min}$  in the case of transient and steady-state.

$$J = -D \frac{\partial c}{\partial z} = -\sqrt{\frac{D}{\pi t}} (c_\infty - c_s) \exp\left(-\frac{z^2}{4Dt}\right)$$



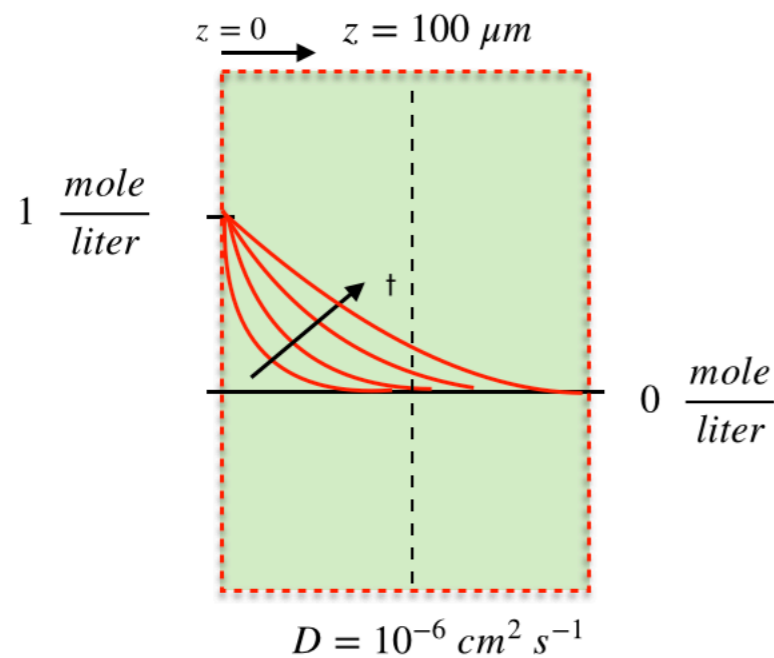
# Exercise 2 solution:

Calculate flux at  $z = 100 \mu\text{m}$  at  $t = 1 \text{ min}$  in the case of transient and steady-state.

$$J = -\sqrt{\frac{D}{\pi t}} (c_\infty - c_S) \exp\left(-\frac{z^2}{4Dt}\right)$$

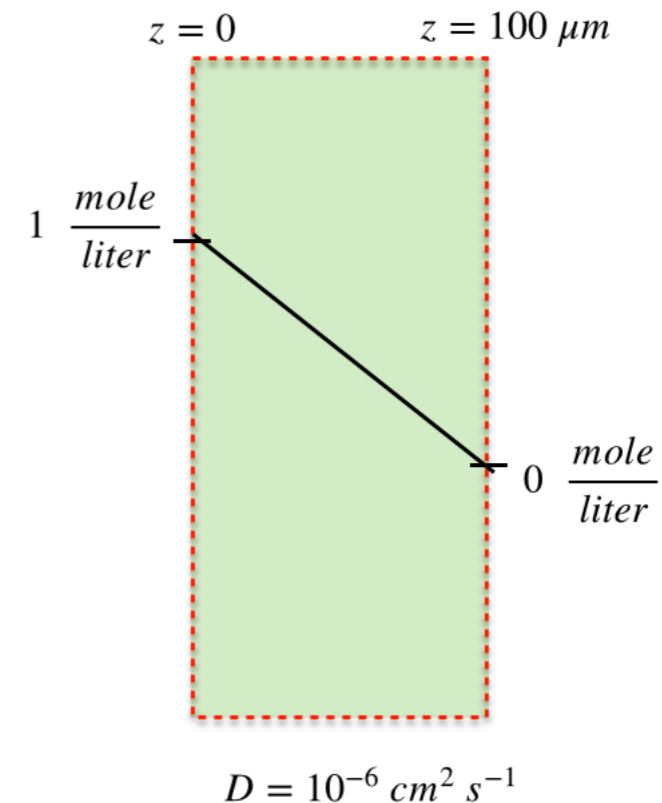
$$J = -\sqrt{\frac{10^{-10}}{\pi 60}} (0 - 1000) \exp\left(-\frac{10^{-8}}{4 * 10^{-10} 60}\right)$$

$$= 4.8 * 10^{-4} \frac{\text{mole}}{\text{m}^2\text{s}}$$



$$J = -D \frac{dc}{dz} = D \frac{(c_0 - c_L)}{L} = \text{constant}$$

$$J = 10^{-10} \frac{(1000 - 0)}{10^{-4}} = 10^{-3} \frac{\text{mole}}{\text{m}^2\text{s}}$$

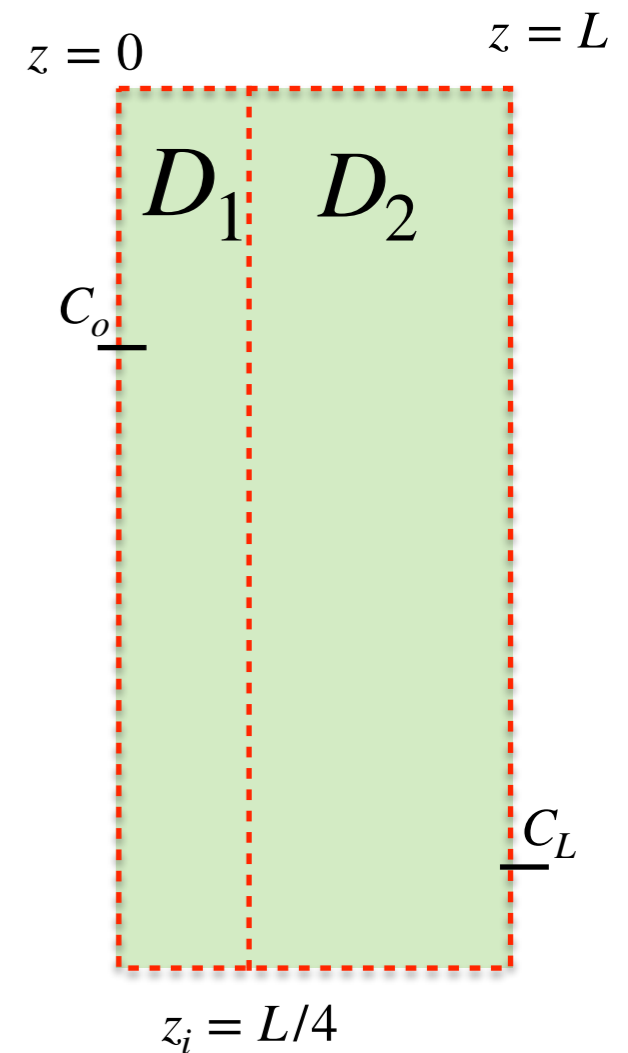


## Exercise 3

Calculate  $c_i$  at the steady-state if  $D_2 = 6D_1$

$$c_o = 10 \text{ mole/L} \quad c_L = 0$$

Draw the concentration profile



## Exercise 3 solution

Calculate  $c_i$  at the steady-state if  $D_2 = 6D_1$

$c_0 = 10 \text{ mole/L}$   $c_L = 0$  Draw the concentration profile

$$J = J_{\text{left}} = J_{\text{right}}$$

$$-D_1 \frac{(c_0 - c_i)}{z_i} = -D_2 \frac{(c_i - c_L)}{z_L - z_i}$$

$$\Rightarrow c_0 - c_i = (c_i - c_L) \left( \frac{D_2}{D_1} \frac{z_i}{z_L - z_i} \right)$$

$$= (c_i - c_L) \left( \frac{D_2}{3D_1} \right) = 2(c_i - c_L)$$

$$\Rightarrow 3c_i = c_0 + 2c_L$$

$$\Rightarrow c_i = c_0/3 = 10/3 \text{ mole/L}$$

